Finite Element Simulation of a Blast Containment Cylinder Using LS-DYNA

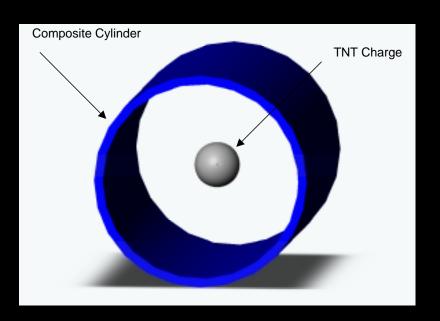
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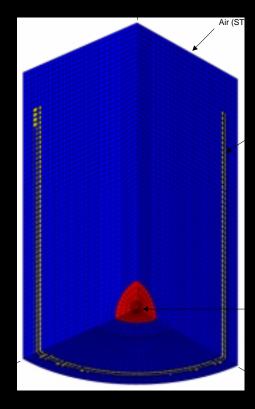
- Several computational models and mesh geometries were created to study blast loading in a containment cylinder.
- To reduce the complexity of the model, Titanium Boride was used as the material for the cylinder instead of a composite material.
- ALE multi-material was used to simulate TNT and air interaction with the cylinder

Introduction



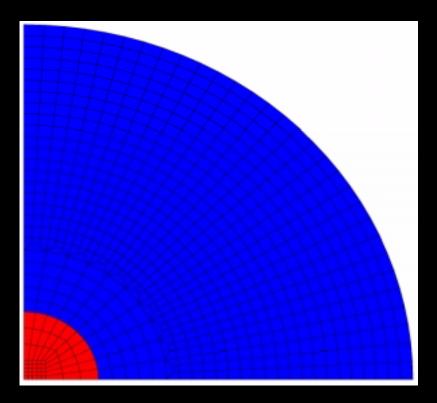
- Cylinder Material, Titanium Boride with an inner radius of 75mm and an outer radius of 81.1mm. The cylinder is 300mm in length
- TNT charge equivalent to 37.4 grams of 50:50 by weight trotyl-hxogen centered in cylinder

Modeling Procedure



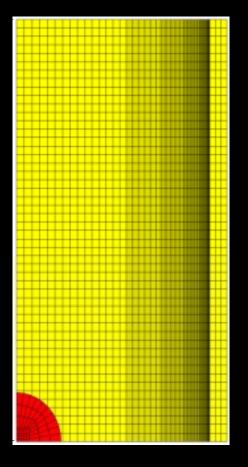
- LS-DYNA was used as the non-linear finite element solver
- TrueGrid was used to generate the mesh
- HyperMesh was implemented to generate the input deck

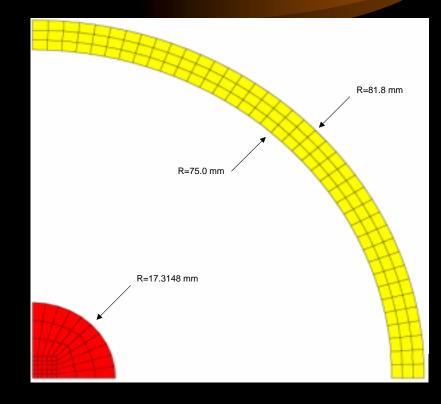
Mesh Geometry



- Element sizes were targeted for 3±2mm with an aspect ratio of 1:1
- To achieve the 3mm target the mesh was transition close to the TNT charge

Side and Bottom Profile







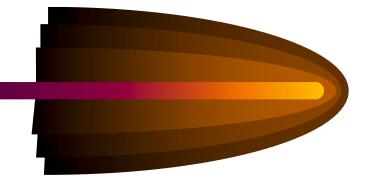
The Jones-Wilkins-Lee (JWL) equation of state (EOS) model for explosive detonation products is given by

$$P = A\left(1 - \frac{\omega}{R_1 V}\right)e^{-R_1 V} + B\left(1 - \frac{\omega}{R_2 V}\right)e^{-R_2 V} + \frac{\omega E}{V}$$

where *A*, *B*, *C*, *R*₁, *R*₂, and ω are constants to be calibrated experimentally, $V = \frac{v}{v_0}$ is the product volume relative to the initial explosive volume, *E* is the energy per unit

volume, and P is the pressure. Values for these constants can be developed experimentally or can be found in the literature.

Linear Polynomial



The Linear Polynomial EOS for linear internal energy is given by

$$P = C_0 + C_1 \mu + C_2 \mu^2 + C_3 \mu^3 + (C_4 + C_5 \mu + C_6 \mu^2) E_0$$

where $C_1 \cdots C_6$ are polynomial coefficients, $\mu = \frac{\rho}{\rho_0} - 1$ with $\frac{\rho}{\rho_0}$ being the ratio of current

density to the initial density, and E has units of pressure. For the modeling of gasses, the gamma law equation of state can be used. This implies that

$$C_0 = C_1 = C_2 = C_3 = C_6 = 0$$

and

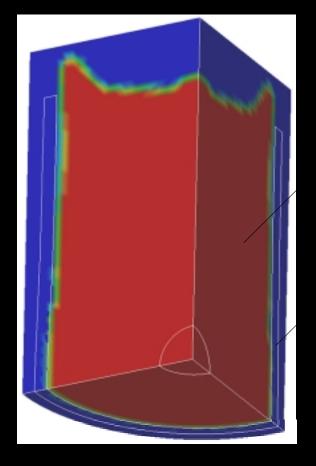
$$C_4 = C_5 = \gamma - 1$$

where γ is the ratio of specific heats. Thus for air the pressure equations is given by

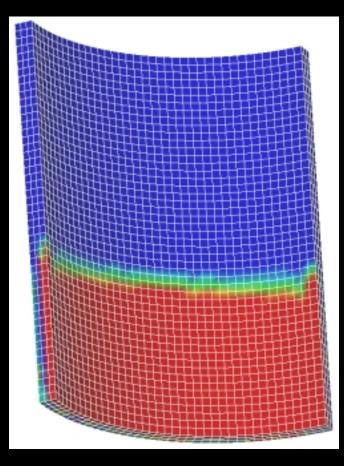
$$p = (\gamma - 1) \frac{\rho}{\rho_0} E$$

It should be noted that for an ideal gas it may be incorrect to assume $C_4 = C_5 = \gamma - 1$ and $C_0 = 0$. The EOS equation should be used in its entirety to check the pressure value.

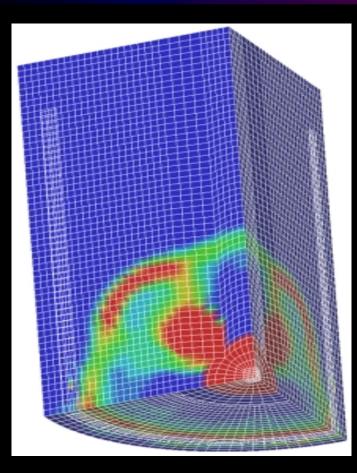
Results



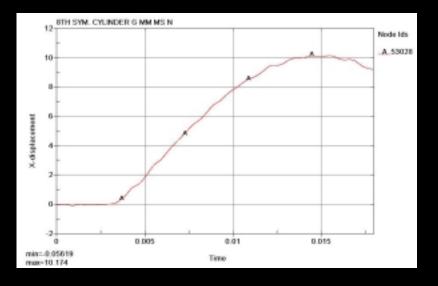
• By changing the penalty factor (PFAC) in the Constrained Lagrange In Solid input card the penetration of the TNT/Air volume fraction into the cylinder mesh can be controlled



 By using different meshes an even pressure loading on the cylinder can be obtained

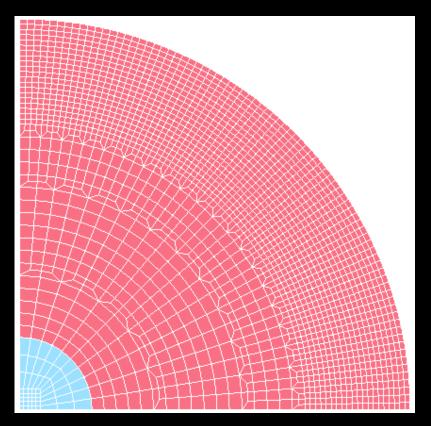


 Transition from spherical to square mesh produces a faster moving and more concentrated pressure wave

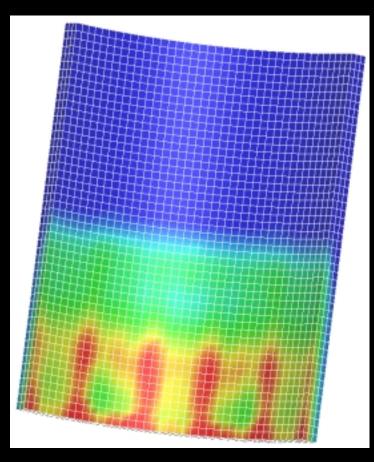


 Pressure wave oscillations can be seen in small oscillations in the displacement plot.

Other Mesh Models



- Multiple Mesh Transitions
- This mesh produces concentrated pressure loading on the cylinder



 Concentrated pressure loading, corresponds to the mesh transitions shown in the previous figure

Future Work

- Mesh geometry studies
- Compare JWL and JWLB peak overpressure for TNT
- Develop composite material models for cylinder
- Compare models with theoretical pressure calculations
- Compare models with experimental data

LS-DYAN Run Information

Memory required for Additional dynamica	lly allocated me		19757935 128903 19886838	
Timing inf	ormation CPU(seconds)		Clock(seconds)	%Clock
Initialization	 7.0000E+00	0.11	7.0310E+00	0.11
Element processing	5.2730E+03	86.22	5.2727E+03	86.21
Binary databases .	3.4000E+01	0.56	3.5167E+01	0.57
ASCII database	1.7000E+01	0.28	1.6758E+01	0.27
Contact algorithm	7.8500E+02	12.84	7.8471E+02	12.83
Contact entities .	0.0000E+00	0.00	0.0000E+00	0.00
Rigid bodies	0.0000E+00	0.00	6.4000E-02	0.00
Implicit Nonlinear	0.0000E+00	0.00	0.0000E+00	0.00
Implicit Lin. Alg.	0.0000E+00	0.00	0.0000E+00	0.00
Totals	6.1160E+03	100.00	6.1164E+03	100.00
Problem time	= 2.0001E-02			
Problem cycle	= 9784			
Total CPU time	= 6116 seco	onds (1 h	ours 41 minutes	56 sec
CPU time per zone c	ycle = 1363	1 nanose	conds	
Clock time per zone	cycle= 1363	2 nanose	conds	
Number of CPU's	2			
Start time 10/30/	2003 12:08:48			
End time 10/30/	2003 13:50:51			
Elapsed time 61	23 seconds (1	hours 4	2 minutes 3 se	conds)



- Gilbert Kinney, Kenneth Graham, 1985, *Explosive Shocks in Air*, Springer-Verlag, ISBN 0-387-15147-9, 3-540-15147-8
- P. D. Smith, J. G. Hetherington, 1994, *Blast and Ballistic Loading of Structures*, ISBN 0-7506-2024-2
- J. A. Zukas, W. P. Walters, 1998, *Explosive Effects and Applications*, Springer-Verlag, ISBN 0-387-98201-9
- 2003, *LS-DYNA Kewords User's Manual Version 970*, Livermore Software Technology Corporation
- MatWeb, *Material Property Data*, www.matweb.com